

How to model the Surface boundary Layer and/or canopy processes?

with a 1D turbulence scheme inside Surface schemes !

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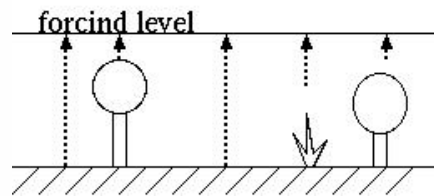
CENTRE NATIONAL
DE LA RECHERCHE
SCIENTIFIQUE



METEO FRANCE
Toujours un temps d'avance

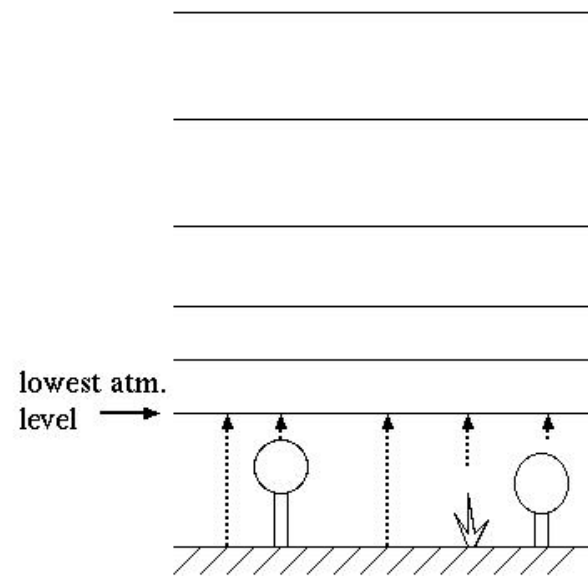
SBL scheme principle : state of the art

a)



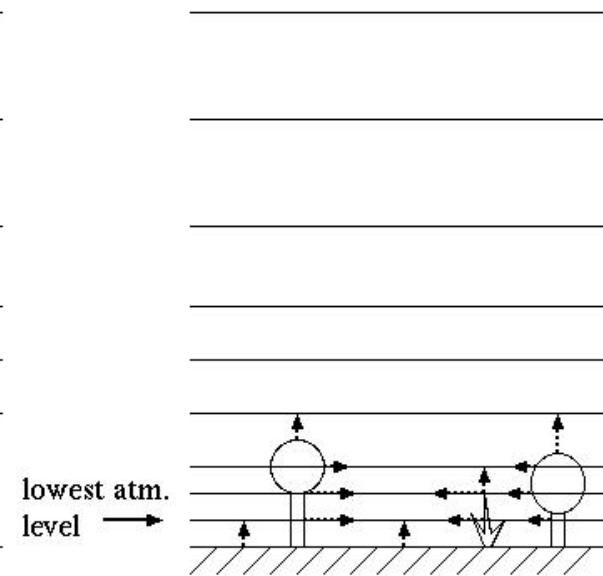
"single-layer" surface
scheme forced off-line

b)



"single-layer" surface scheme
coupled to an atmospheric model

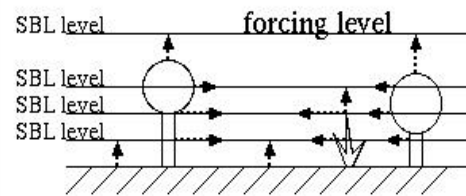
c)



"multi-layer" surface scheme
coupled to an atmospheric
model

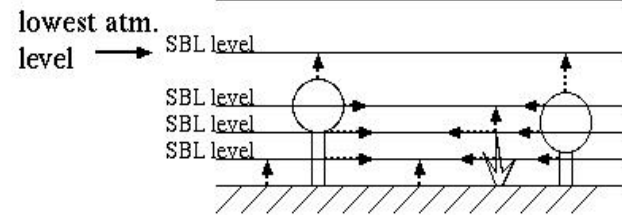
SBL scheme principle : what we want to do

a)



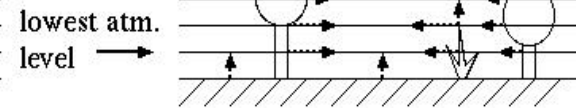
"single-layer" surface scheme
+ Surface Boundary Layer scheme
forced offline

b)



"single-layer" surface scheme
+ Surface Boundary Layer scheme
coupled to an atmospheric model

c)



"multi-layer" surface scheme
coupled to an atmospheric
model

SBL & « canopy » scheme

- Evolution equations in the SBL are :

$$\left\{ \begin{array}{l} \frac{\partial U}{\partial t} = Adv + Cor + Pres. + Turb(U) + Drag_u \\ \frac{\partial V}{\partial t} = Adv + Cor + Pres. + Turb(V) + Drag_v \\ \frac{\partial \theta}{\partial t} = Adv + Diab. + Turb(\theta) + \frac{\partial \theta}{\partial t} canopy \\ \frac{\partial q}{\partial t} = Adv + Turb(q) + \frac{\partial q}{\partial t} canopy \end{array} \right.$$

$$\frac{\partial e}{\partial t} = Adv + Dyn.Prod. + Therm.Prod. + Turb + Diss. + \frac{\partial e}{\partial t} canopy$$

SBL & « canopy » scheme

- Regrouping terms into 3 main types :

$$\left\{ \begin{array}{l} \frac{\partial U}{\partial t} = LS(U) + Turb(U) + Drag_u \\ \frac{\partial V}{\partial t} = LS(V) + Turb(V) + Drag_v \\ \frac{\partial \theta}{\partial t} = LS(\theta) + Turb(\theta) + \frac{\partial \theta}{\partial t}_{canopy} \\ \frac{\partial q}{\partial t} = LS(q) + Turb(q) + \frac{\partial q}{\partial t}_{canopy} \end{array} \right.$$

The TKE equation remains the same:

$$\frac{\partial e}{\partial t} = Adv(e) + Dyn.Prod. + Therm.Prod. + Turb + Diss. + \frac{\partial e}{\partial t}_{canopy}$$

SBL & « canopy » scheme

- Supposing that:
 - The mean wind direction does not vary with height in the SBL
 - The turbulent transport and advection of TKE is small in the SBL compared to other terms
 - Above the canopy (if any), the turbulent fluxes are uniform with height (« constant flux layer »)
 - The Large-Scale Forcing terms $LS(U)$, $LS(\theta)$, $LS(q)$ are uniform with height in the SBL
- These are hypotheses commonly done in Monin-Obukhov-like SBL relationships

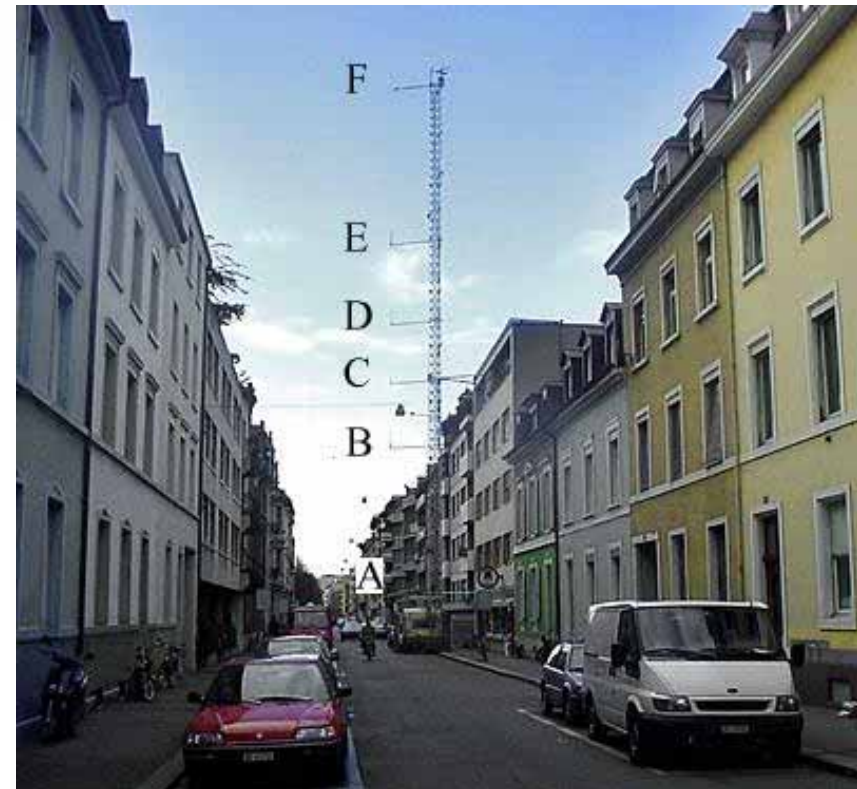
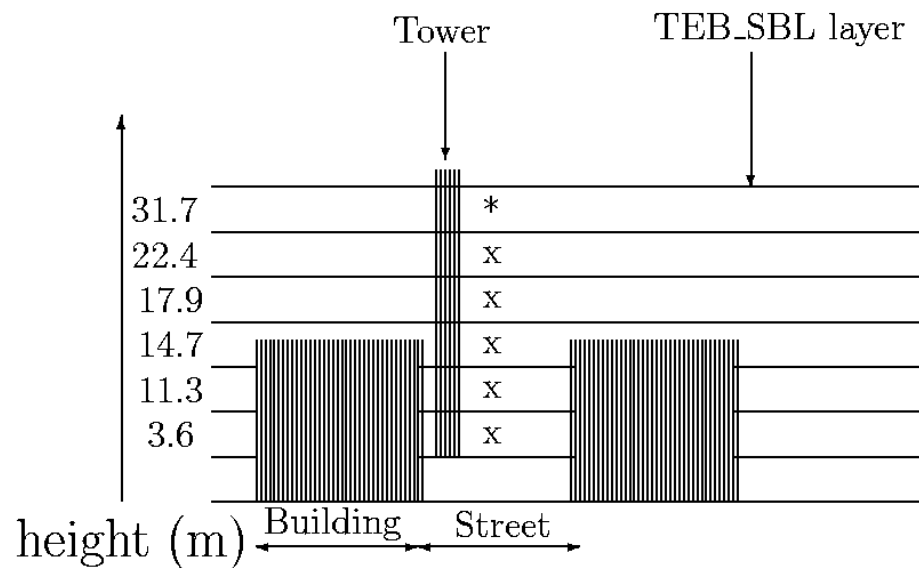
$$\left\{ \begin{array}{l} \frac{\partial U}{\partial t} = \frac{\partial U}{\partial t}(z = z_a) + Turb(U) + Drag_u \\ \frac{\partial \theta}{\partial t} = \frac{\partial \theta}{\partial t}(z = z_a) + Turb(\theta) + \frac{\partial \theta}{\partial t}_{canopy} \\ \frac{\partial q}{\partial t} = \frac{\partial q}{\partial t}(z = z_a) + Turb(q) + \frac{\partial q}{\partial t}_{canopy} \end{array} \right.$$

$$\frac{\partial e}{\partial t} = Dyn.Prod. + Therm.Prod. + Diss. + \frac{\partial e}{\partial t}_{canopy}$$

SBL canopy scheme in TEB

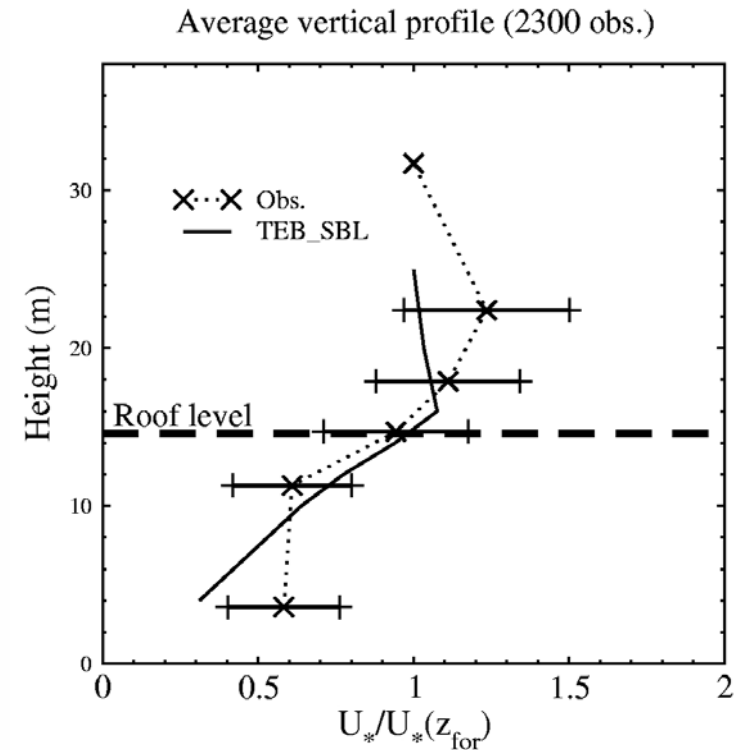
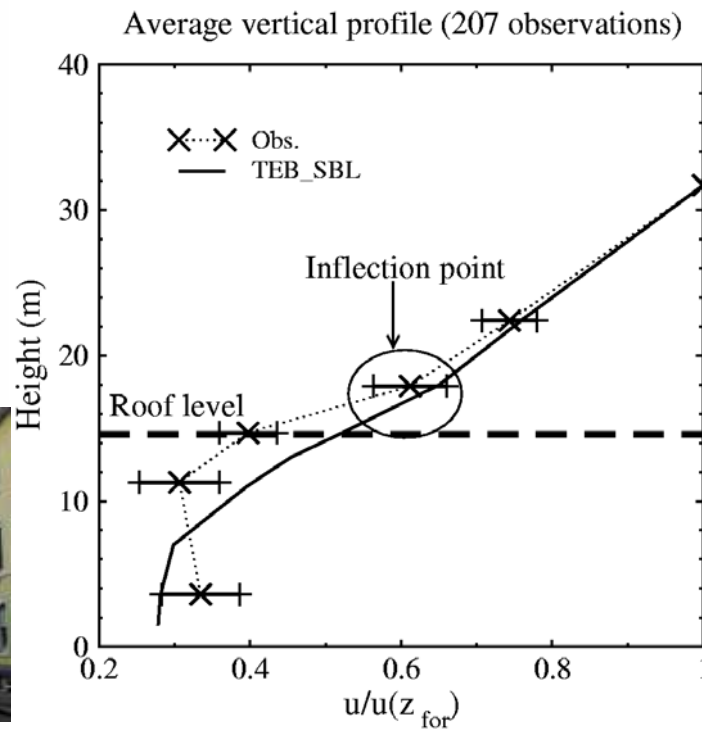
- Offline Validation with the BUBBLE data
 - City-center of Basel (Switzerland)
 - Simulation covers half of the summer IOP: from 16th to 30th June, 2002

Basel-Sperrstrasse



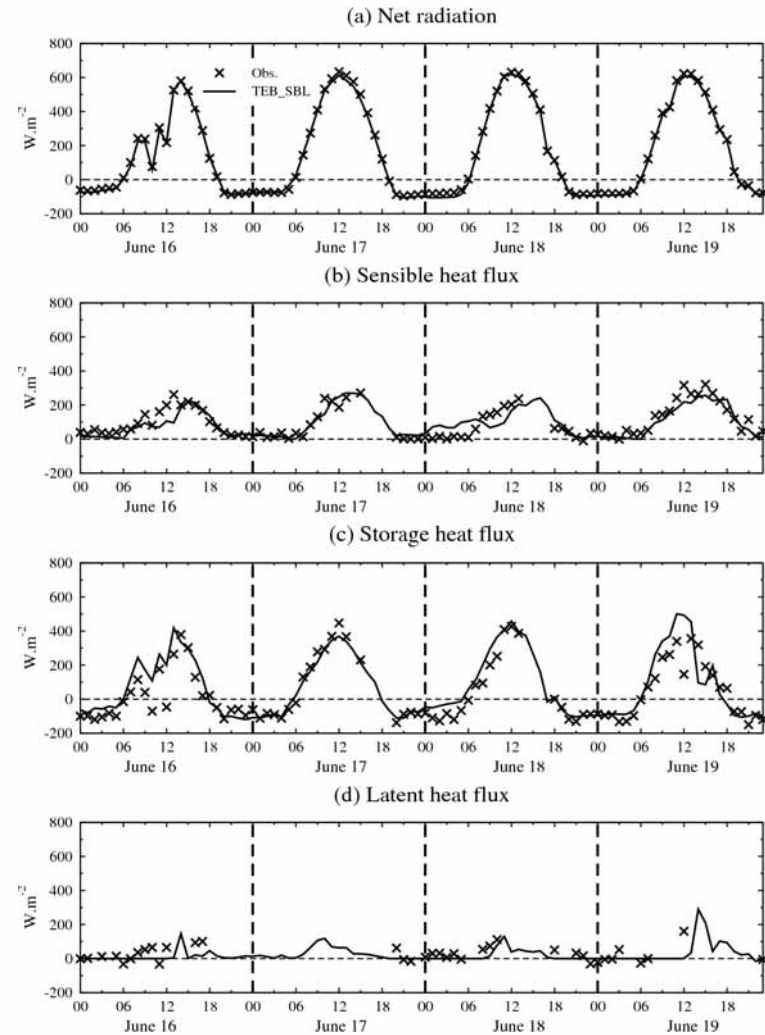
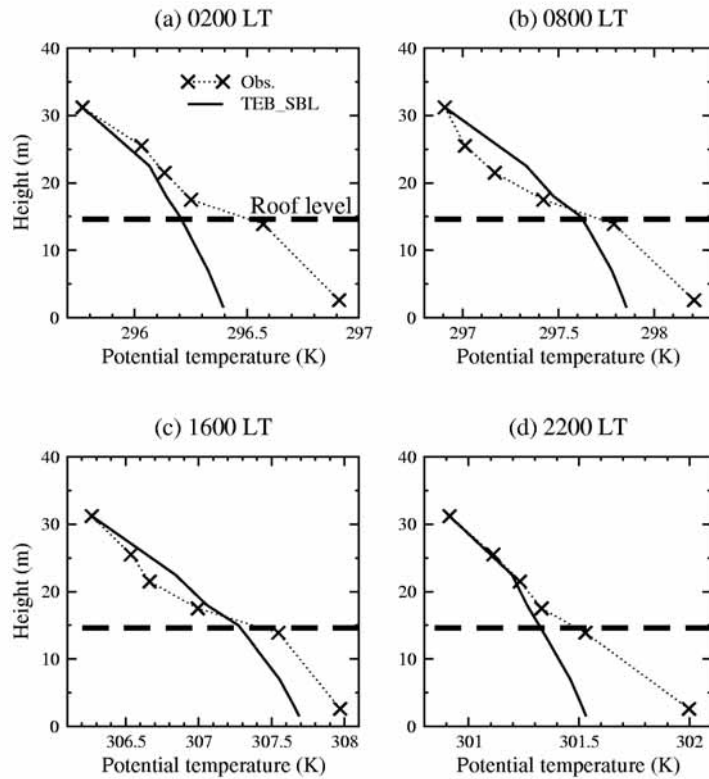
SBL canopy scheme in TEB

- Dynamical variables
 - Walls imply a drag force on the flow parameterized ($CD=0.4$) as : - $Cd U^2$
 - Walls are also a source of TKE, parameterized as : + $Cd U^3$
 - Both mean wind profile and momentum fluxe profile are correctly simulated



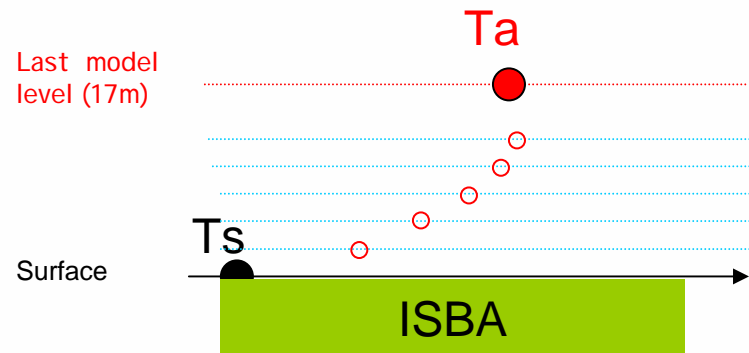
SBL canopy scheme in TEB

- Temperature and surface Energy Budget
 - Heating terms come from wall, roof, road separate energy budgets
 - Good fluxes, temperature profile good above roof level, could be improved near the road



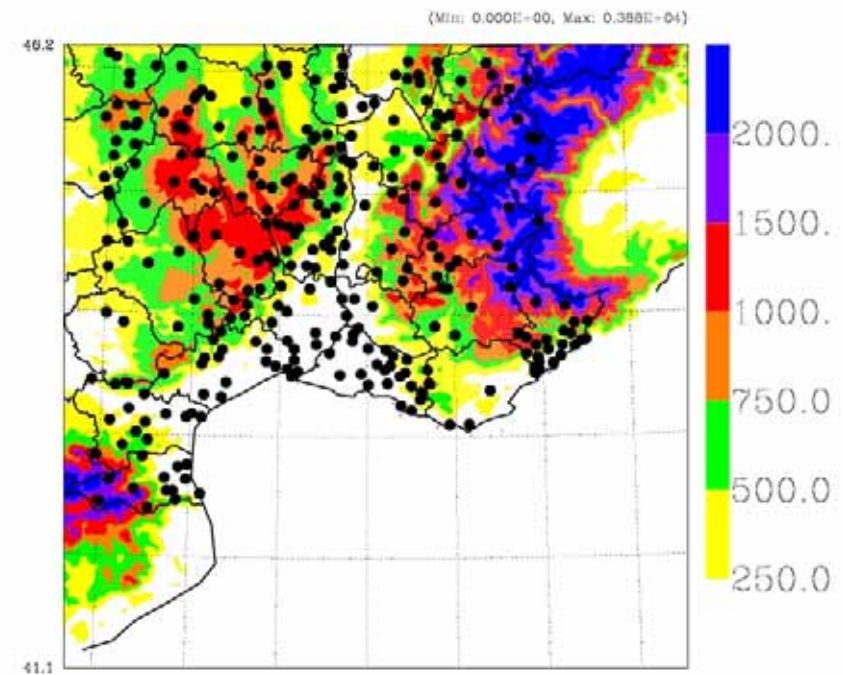
Evaluation in AROME

Surface Boundary Layer



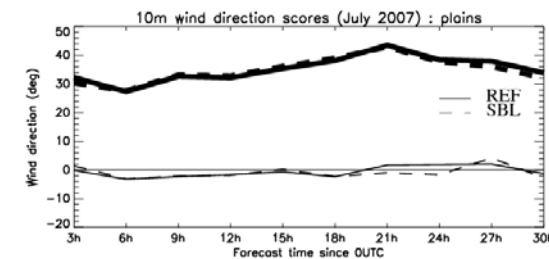
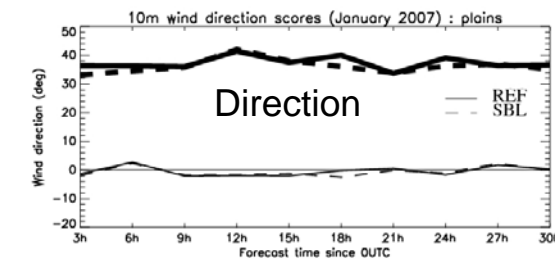
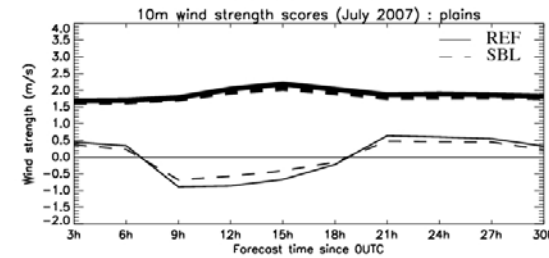
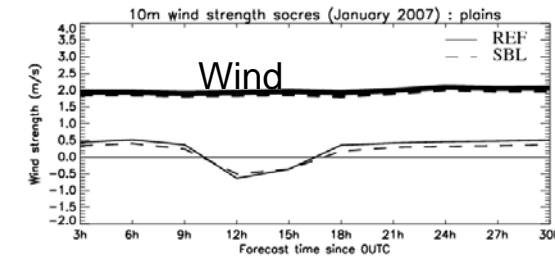
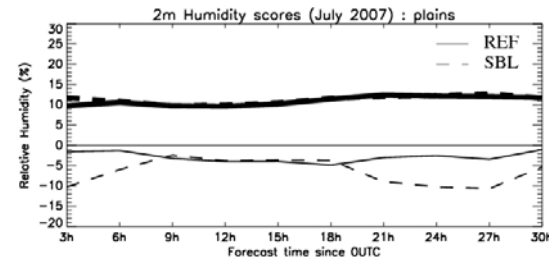
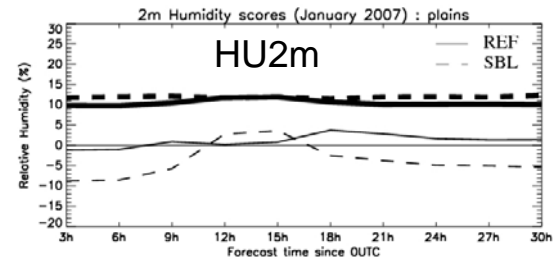
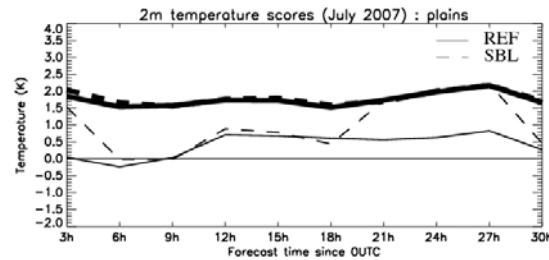
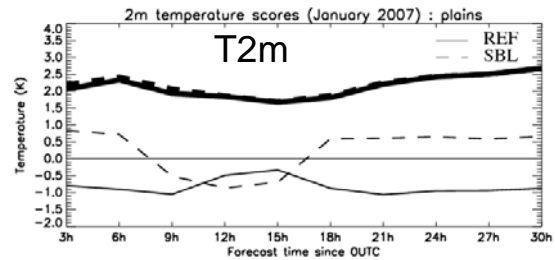
5 levels added +
turbulence scheme used

Evaluation on July 2007 and January 2007 on South East France domain :



Evaluation in AROME

- Scores in plains ($z < 300\text{m}$)



- SBL better in January, worse in July

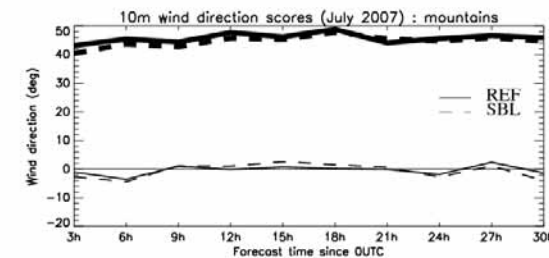
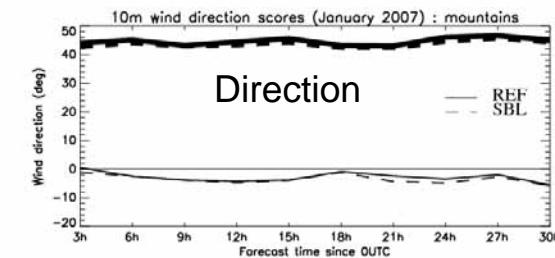
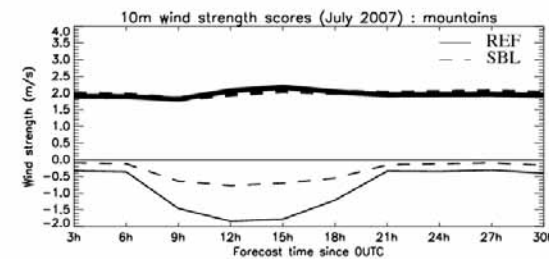
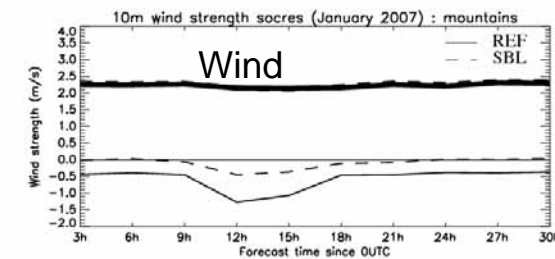
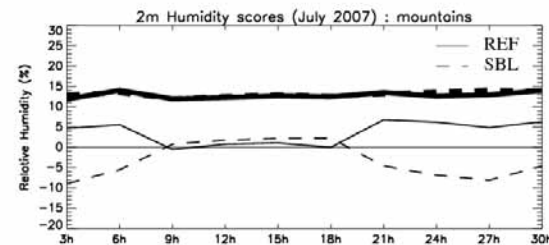
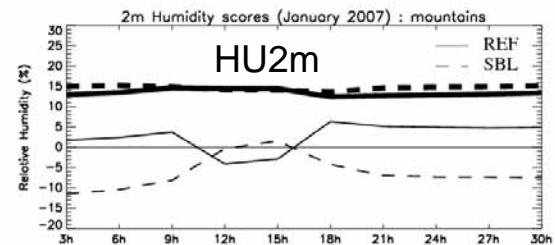
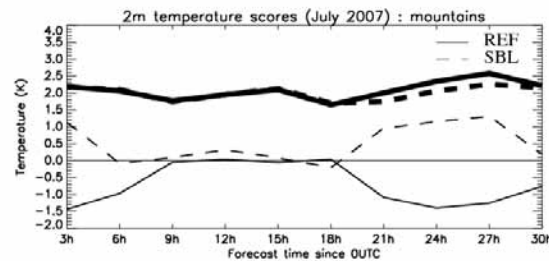
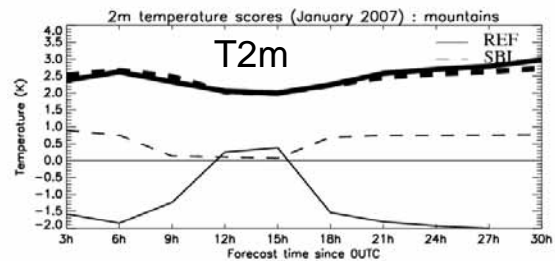
- Reflects t2m errors

- SBL better for wind strength

- SBL better for wind direction (even if wind direction is not a SBL scheme variable !)

Evaluation in AROME

- Scores in mountaineous areas



- SBL better in January & July
- Reflects t2m errors
- SBL better for wind strength
- SBL better for wind direction (even if wind direction is not a SBL scheme variable !)

Evaluation in AROME

Better statistical scores,
Especially in mountains

No surface/atmosphere decoupling



Significant (negative) heat fluxes



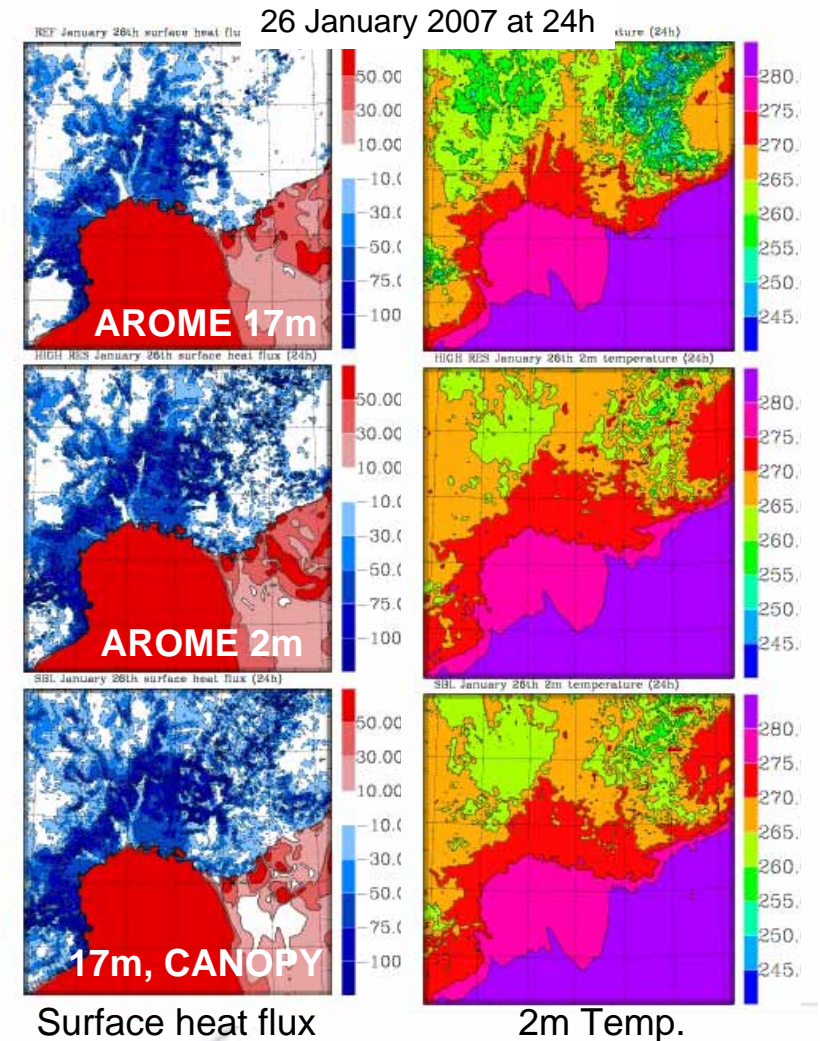
Air cooling in the atmospheric model



Better catabatic winds



Better structure of temperature field



Conclusions

- One 1D SBL & « canopy » scheme has been included in SURFEX
- This allows a better physical treatment of the SBL, taking into account obstacle effects if any (e.g. buildings in TEB)
- Scores are globally improved, especially over mountains
- To couple the surface scheme (ISBA) with a very low SBL level avoids the classical surface/atmosphere decoupling
- Opens new collaboration opportunities on e.g. forest schemes including a tree canopy

Conclusions

- Thank you

SBL & « canopy » scheme

- Turbulence scheme is the Cuxart, Bougeault, Redelsperger (2000)
- Mixing and dissipative length scale, above canopy, are given by Redelsperger, Mahé and Carlotti 2001

A summary of the turbulence scheme is given below:

$$\left\{ \begin{array}{l} \overline{u'w'} = -C_u l \sqrt{e} \frac{\partial U}{\partial z} \\ \overline{w'\theta'} = -C_\theta l \sqrt{e} \frac{\partial \theta}{\partial z} \\ \overline{w'q'} = -C_q l \sqrt{e} \frac{\partial q}{\partial z} \\ \frac{\partial e}{\partial t} = \underbrace{-\overline{u'w'} \frac{\partial U}{\partial z}}_{\text{Dyn.Prod.}} + \underbrace{\frac{g}{\theta} \overline{w'\theta'}}_{\text{Therm.Prod.}} - \underbrace{C_\epsilon \frac{e^{\frac{3}{2}}}{l_\epsilon}}_{\text{Diss.}} + \frac{\partial e}{\partial t}_{\text{canopy}} \end{array} \right. \quad (10)$$

with $C_u = 0.126$, $C_\theta = C_q = 0.143$, $C_\epsilon = 0.845$ (from Cheng et al 2002 constants values for pressure correlations terms and using Cuxart et al 2000 derivation). The mixing and dissipative lengths, l and l_ϵ respectively, are equal to (from Redelsperger et al 2001, $\alpha = 2.42$):

$$\left\{ \begin{array}{ll} l = \kappa z / [\sqrt{\alpha} C_u \phi_m^2(z/L_{MO}) \phi_e(z/L_{MO})]^{-1} & \\ l_\epsilon = l \alpha^2 C_\epsilon / C_u / (1 - 1.9z/L_{MO}) & \text{if } z/L_{MO} < 0 \\ l_\epsilon = l \alpha^2 C_\epsilon / C_u / (1 - 0.3\sqrt{z/L_{MO}}) & \text{if } z/L_{MO} > 0 \end{array} \right. \quad (11)$$

Where L_{MO} is the Monin-Obukhov length, ϕ_u and ϕ_e the Monin-Obukhov stability functions for momentum and TKE.